

Solar Thermal Absorber Coatings



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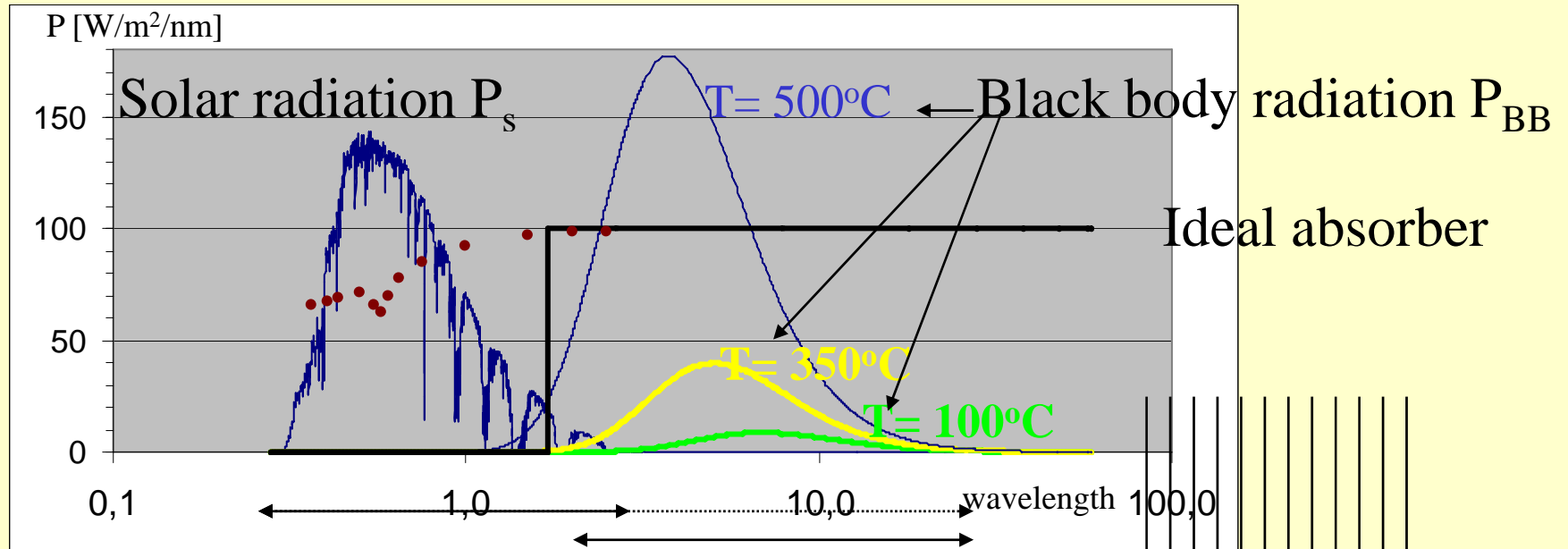
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- Ongoing development of Thermal Absorber Coating for elevated temperatures
 - Process stability
 - Testing procedure
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Outline

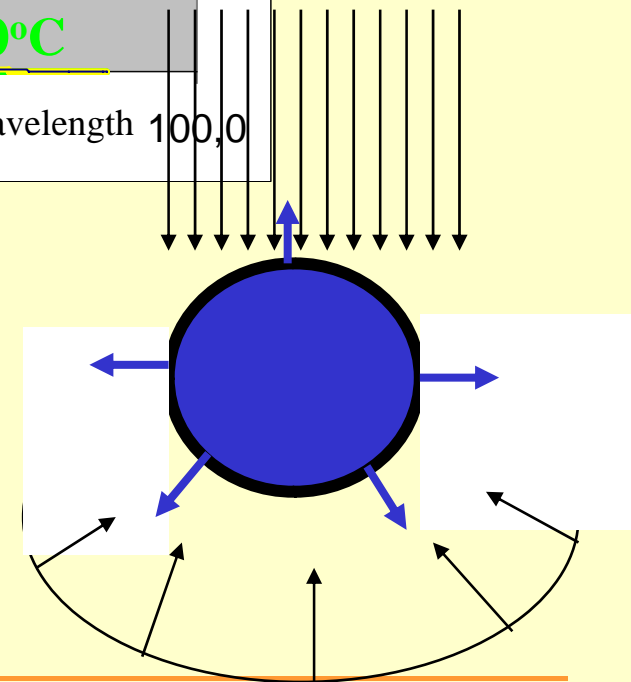
1. Coating properties
 2. Existing solutions
 1. Paint
 2. Electrochemical black Cr /Ni
 3. **PVD / PECVD multilayered coating**
 3. Coating development
 1. Process stability
 4. Thermal Testing
 1. Degradation mechanism
 2. Flat panel collector
 3. Vacuum tube collector
 5. Summary
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Goal for coating properties (1)



Optical (reflection)
measurements

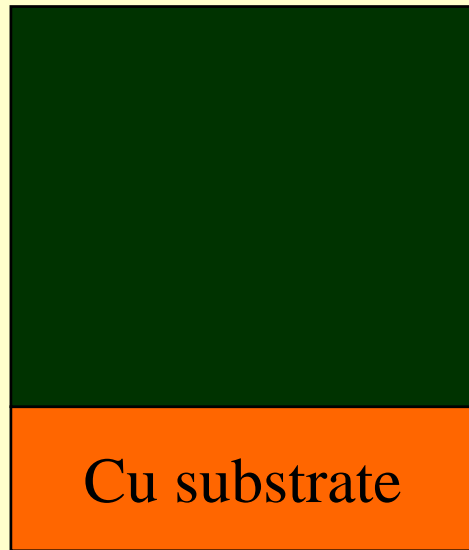
Global emission at
working temperature
(emissometer)



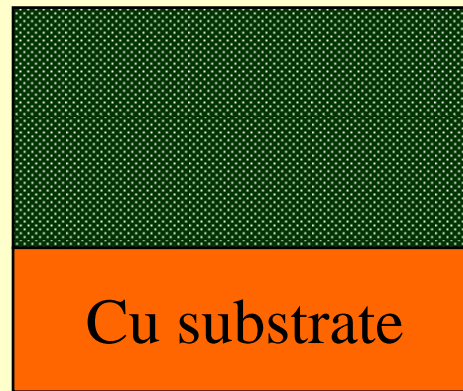
$$\alpha = \int a(\lambda) p_s(\lambda) d\lambda$$

$$\varepsilon = \int a(\lambda) p_{BB}(\lambda) d\lambda$$

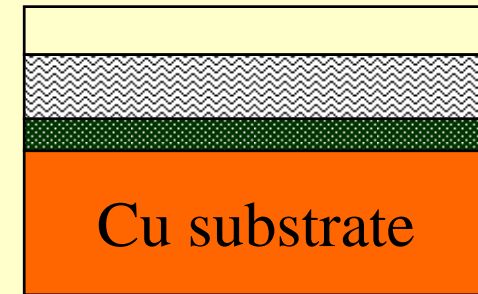
Coating solution (s)



Black paint



Black Cr and Ni
(electrochemical)



multi layer
(PVD, PECVD)

$\alpha = 50 \% \dots 93 \%$

$\varepsilon = 40 \dots 80 \%$

85...95 %

12 %

> 95%

< 5%

Thermal emission during application

Lisbon: $P_s = 2200 \text{ kWh} / \text{y} / \text{m}^2$

Net absorption: $P = P\alpha - P\varepsilon$

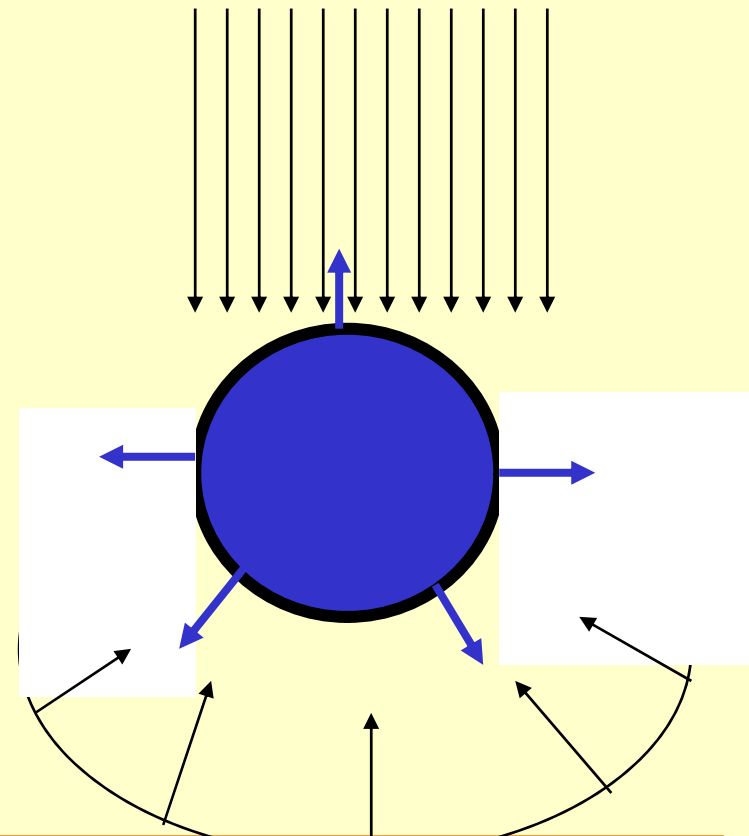
$\$ = 0.1 \text{ €} / \text{Kwh}$

$\alpha = 0.95$

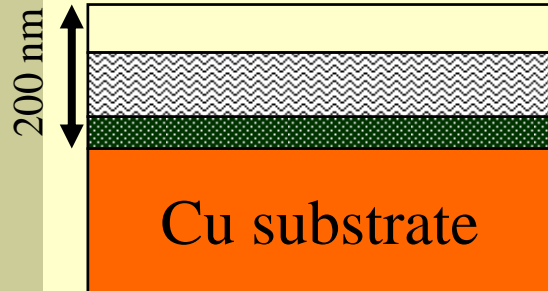
$\varepsilon = 0.07 \dots 0.05$

$P_e = 98 \text{ KWh} \dots 70 \text{ Kwh}$

$\Delta P = 3 \text{ €} / \text{y}$



PVD coating solution (s)



multi-layer PVD

<i>layer3</i>	SiO _x	Si ₃ N ₄	a-C:H	Al ₂ O ₃	SnO ₂ :F
<i>layer2</i>	TiN _x O _y	TiAlN _x O _y	a-C:H/Cr	Al	Cr _x O _y
<i>layer1</i>	TiN (1)	TiAlN (2)	CrC (3)	Al ₂ O ₃ (4)	CrN _x O _y (5)
<i>Diff. barrier</i>	TiC				??
<i>α</i>	95%	96 %	91...95%	90%	95%
<i>ε</i>	5 %	7 %	9...5%	6 %	4...5%

(1) <http://www.tinox.com/>

(2) US20070196670 H.C. Barshilia et.al.

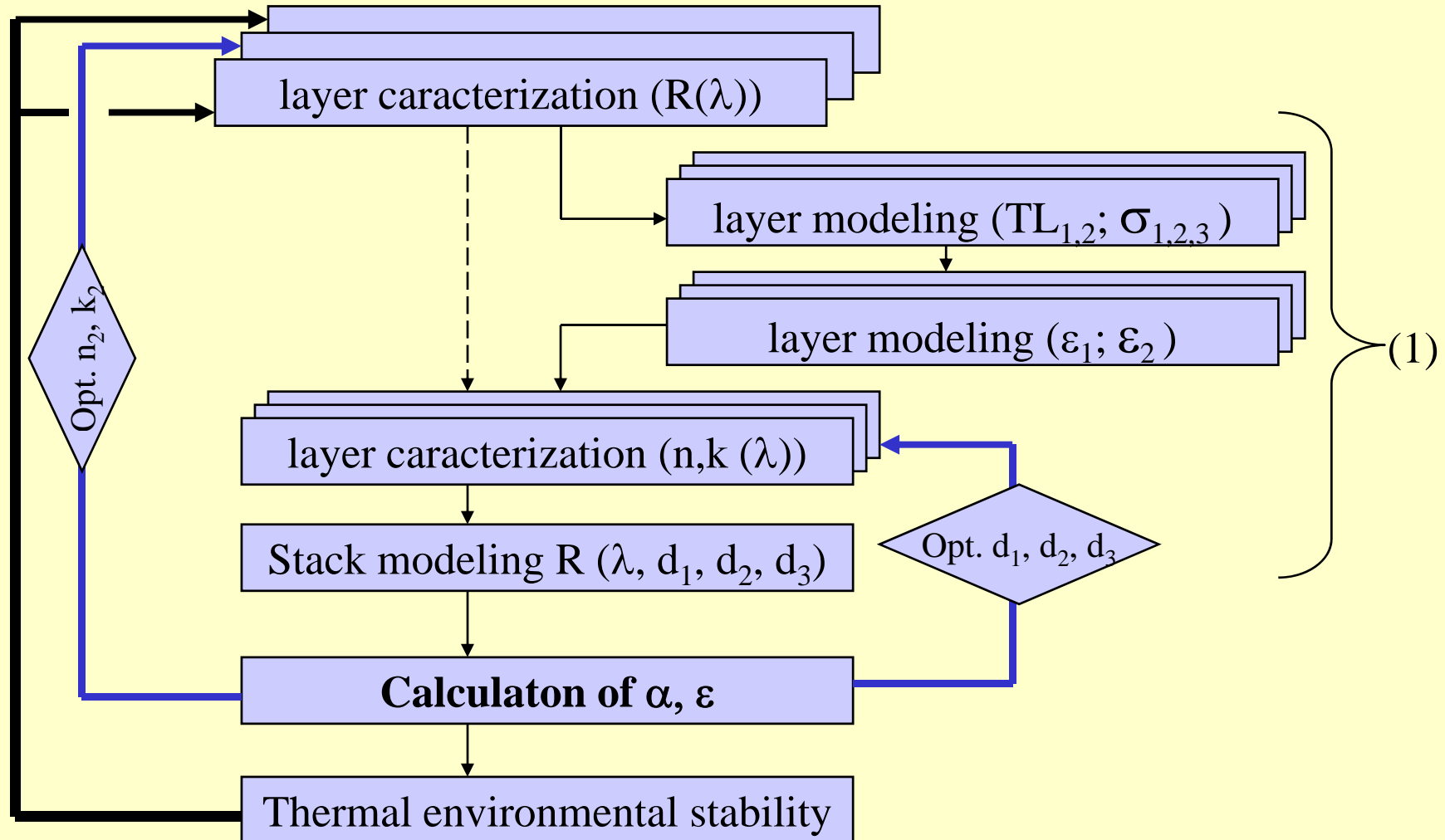
(3) Von Ardenne <http://www.ese.iitb.ac.in/activities/> ; Accelerated aging tests of chromium containing amorphous hydrogenated carbon coatings for solar collectors Solar Energy Materials and Solar Cells 54 (1998) 369-377R. Gampp P. Oelhafen, P. Gantenbein, S. Brunold, U. Frei

(4) Optical properties and thermal stability of pulsed-sputter-deposited Al_xO_y/Al/Al_xO_y multilayer absorber coatings; Solar Energy Materials and Solar Cells, Volume 93, Issue 3, March 2009, Pages 315-323 H C. Barshilia, Net.al

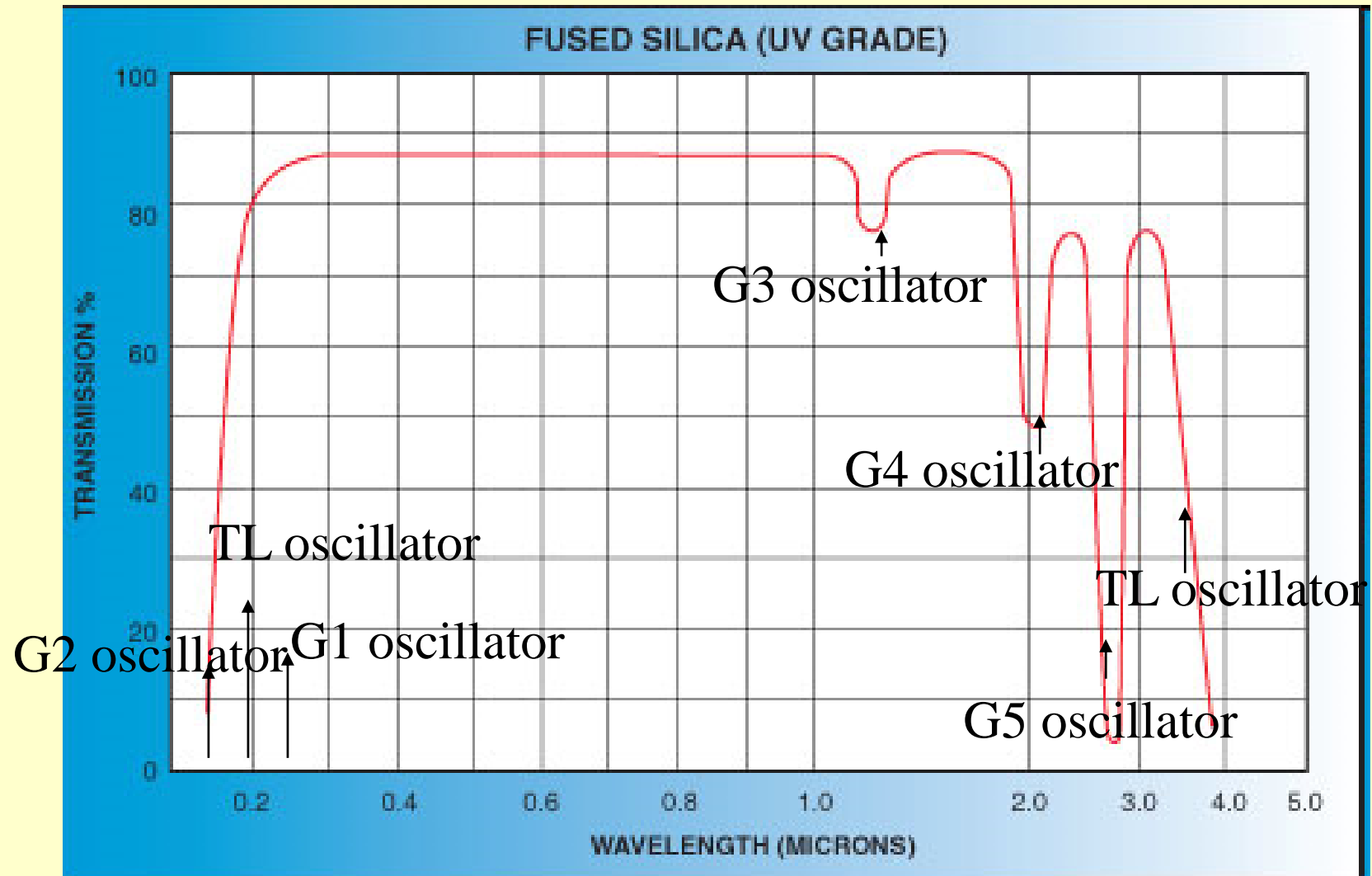
(5) Von Ardenne <http://www.ese.iitb.ac.in/activities/> ;

(6) www.alanod-solar.com , www.bluetec-germany.com

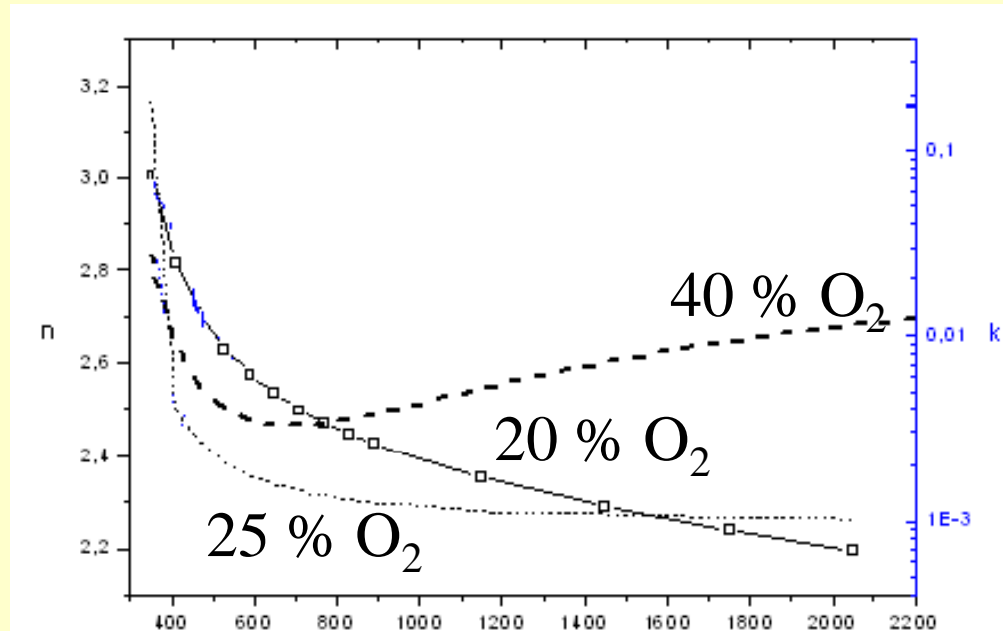
Coating Development



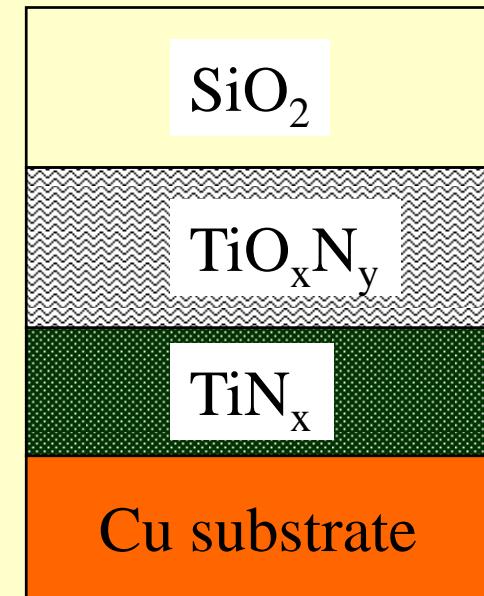
Optical Development (1)



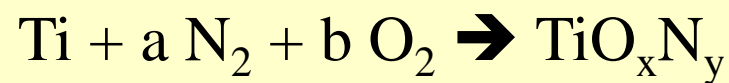
Coating Development (1): TiO_xN_y composition



60 nm
17 nm
30 nm



multi-layer PVD

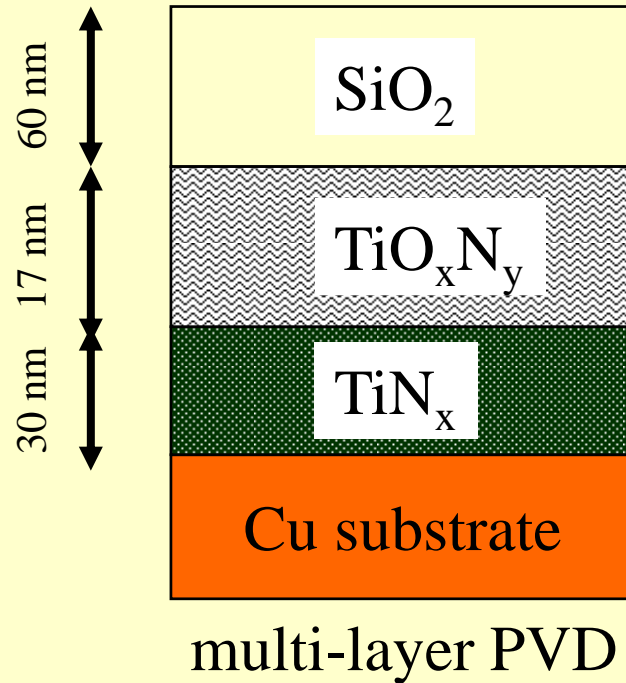


N₂ flow constant

O₂ quantity controlled by plasma emission PE

PE _{O₂}	n _{500nm}	α	ε
20 %	2.7	94 %	6 %
25 %	2.4	93 %	7 %

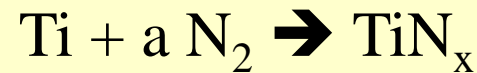
Coating Development (2)



Oxide layer thickness

d ₁	d ₂	d ₃	α	ε
30	17	60	94 %	6 %
30	17	50	89 %	7 %

TiN_x composition



PE _{N₂}	n		α	ε
90 %	3.1		94 %	6 %
80 %	2.8		86 %	7 %

N₂ quantity controlled by plasma emission PE

Degradation mechanism

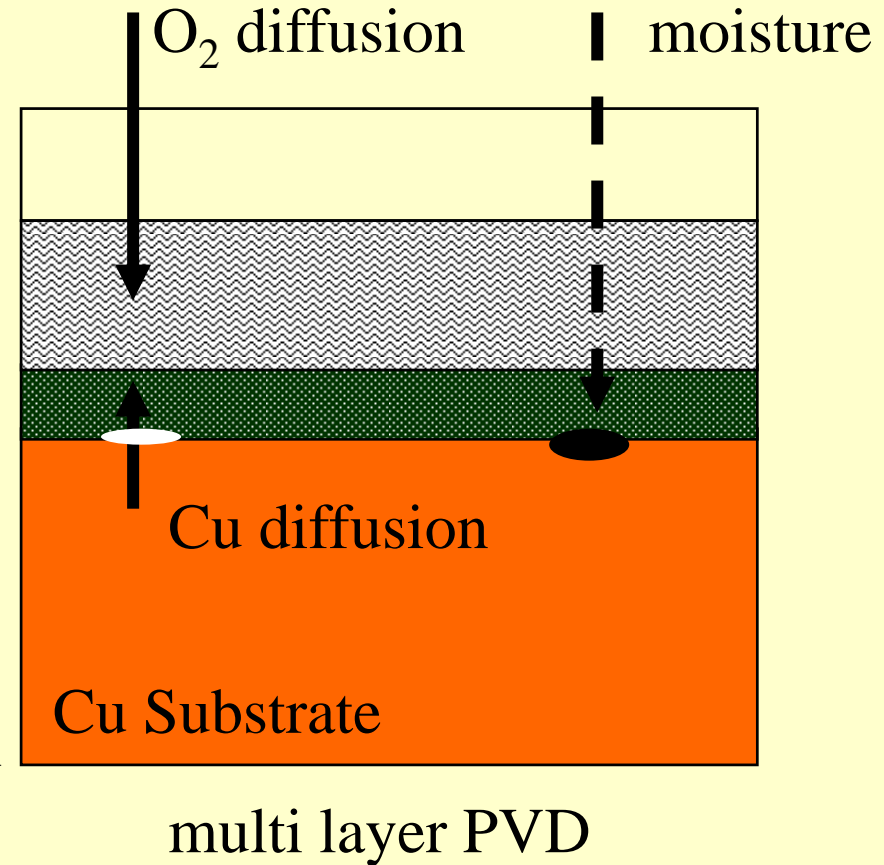
Long term stability
at operation temperature:

PC =

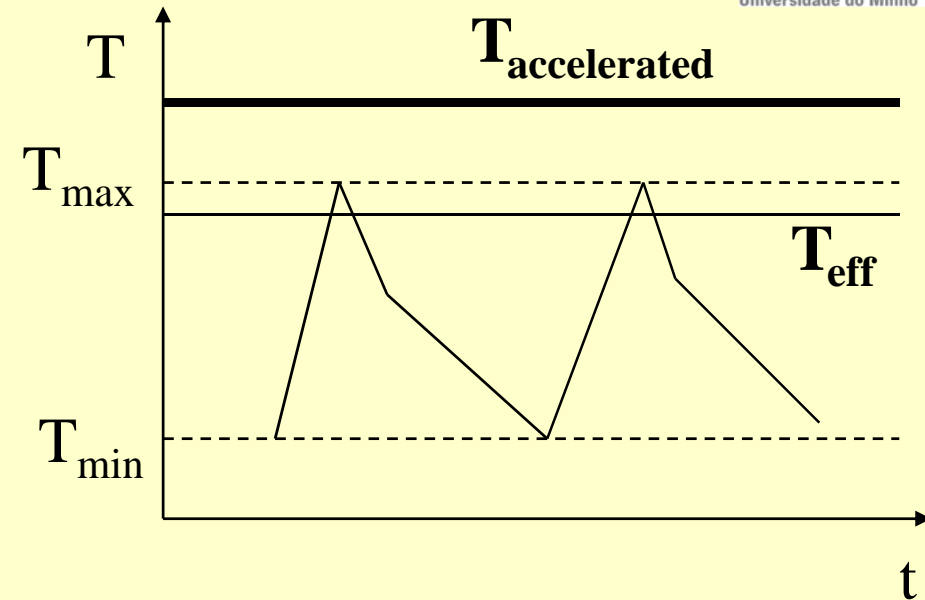
$$-\Delta \alpha + 0.25 \Delta \varepsilon < 0.05$$

no spallation

Thermal
expansion
during thermal
cycling



Accelerated tests (effective temperature)



$$t_{\text{lifetime}} = 25 \text{ y}$$

$$e^{\frac{-E_a}{RT_{\text{eff}}}} = \int_{T_{\text{min}}}^{T_{\text{max}}} e^{\frac{-E_a}{RT}} f(T) dT$$

$$t_{\text{accelerated}} = 25 \text{ ye}^{\frac{-E_a}{R} \left(\frac{1}{T_{\text{eff}}} - \frac{1}{T_{\text{accelerated}}} \right)}$$

Accelerated testing (1)

Long term stability

at low operation temperature ($T_{\text{typical}} < 100^{\circ}\text{C}$) flatpanel collector:

PC =

$$-\Delta \alpha + 0.25 \Delta \varepsilon < 0.05$$

Test procedure (ISO/CD 12592.2):

($T_{\text{stagnation}} = 203^{\circ}\text{C}$, $\alpha = 95\%$, $\varepsilon = 5\%$)

1. Adhesion Test:

Tape test > 0.15 MPa

2. Thermal testing

$T = 278^{\circ}\text{C}$, $t = 36, 75, 150, 300, 600$ h

$T = 308^{\circ}\text{C}$, $t = 141, 342$ h

3. Humidity testing (w/ condensation)

$T = 40^{\circ}\text{C}$; RH = 95 % , $t = 80, 150, 300$ and 600 h

$T = 60^{\circ}\text{C}$; RH = 95 % , $t = 85$ h

4. Additional testing (microclimate)

Accelerated testing (2)

Long term stability

at high operation temperature ($T_{\text{stagnation}} \geq 350^\circ\text{C}$) vacuum tube collector:

$$PC = -\Delta \alpha + 0.25 \Delta \varepsilon < 0.05$$

Test procedure:

($T_{\text{stagnation}} = 350^\circ\text{C}$, $t = 25\,000\text{ h}$ (25 y)

$\alpha = 95\%$, $\varepsilon = 5\%$, $E_A = 190\text{ KJ/mol}$ for

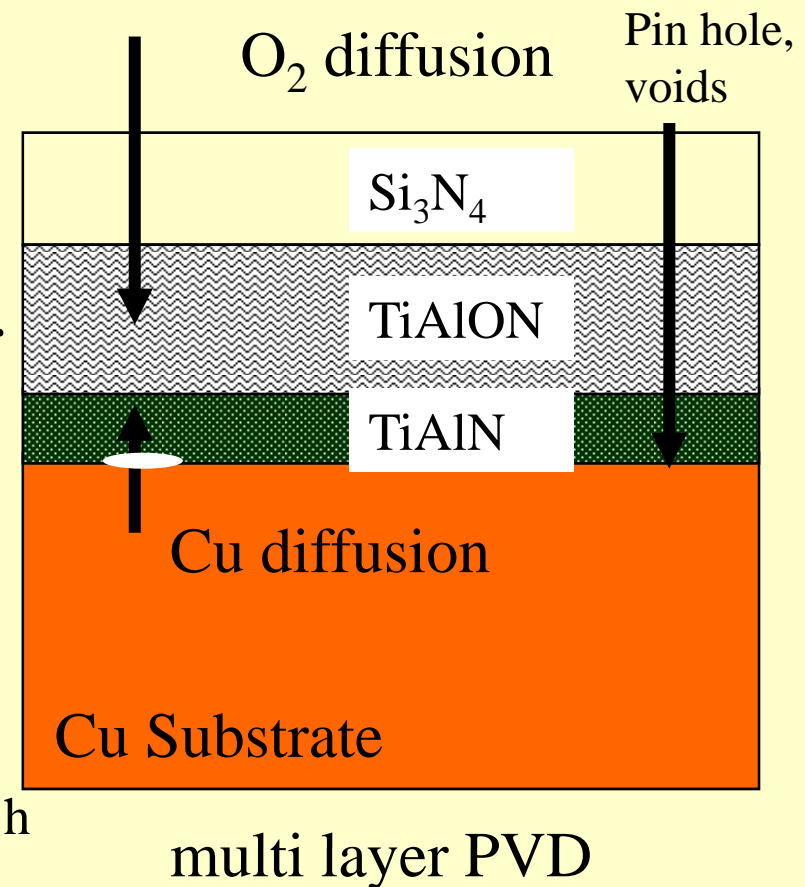
Oxidation)

1. Adhesion Test:

Tape test $> 0.15\text{ MPa}$

2. Thermal testing

$T = 440^\circ\text{C}$, $t = 600\text{ h}$ + $T = 483^\circ\text{C}$, $t = 85\text{ h}$

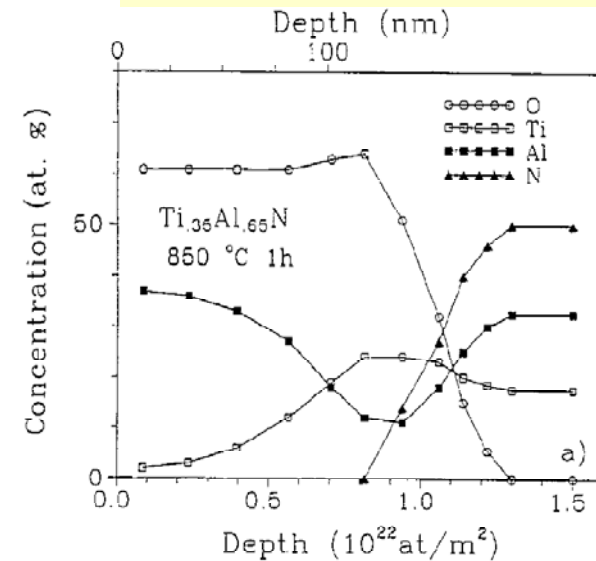
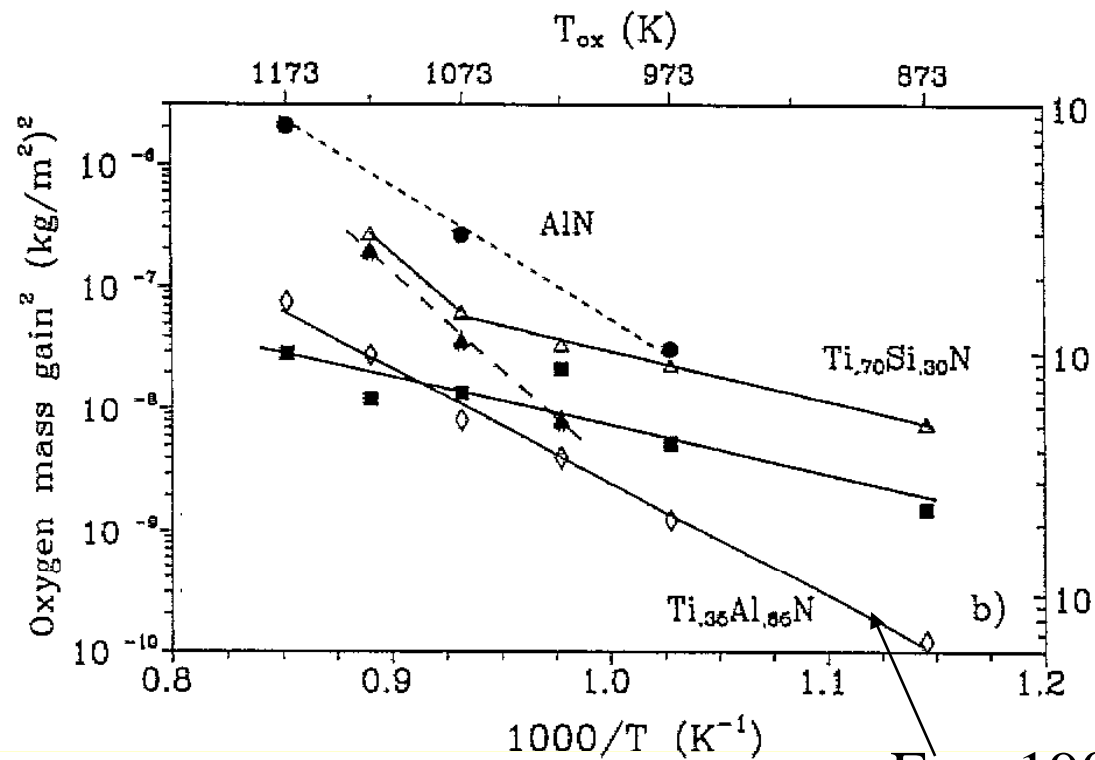


Accelerated tests: diffusion mechanism

Long term stability

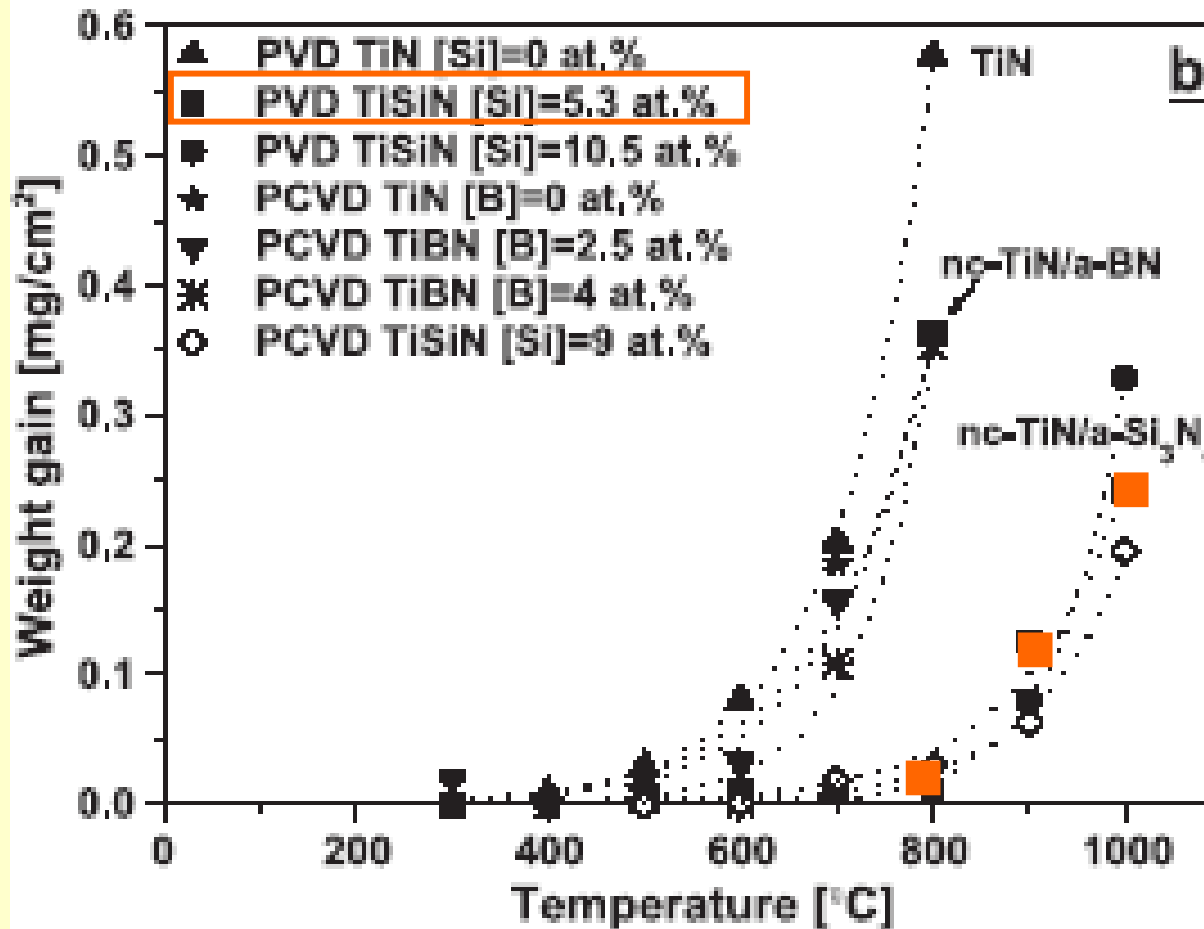
at high operation temperature ($T_{\text{stagnation } T} \geq 350^\circ\text{C}$) vacuum tube collector:

$$PC = -\Delta \alpha + 0.25 \Delta \varepsilon < 0.05$$



$$E_a = 190 \text{ KJ/mol}$$

Growth of oxide layer



$$\Delta m \left[\frac{mg}{cm^2} \right] = \sqrt{k^* t}$$

$$k^* = k_o^* \exp\left(-\frac{E}{RT}\right)$$

→ T = 600°C
 t = 30 000 h
Δd < 15 nm

Summary



- Numerous optical solutions for a high performance ($\alpha > 95 \%$, $\varepsilon < 5 \%$) absorber coating
 - main characteristics: 3 layer PVD coating
 - Elevated temperature degradation controlled by diffusion processes
 - All layers must be stable at application temperature (stagnation temperature)
 - At least one layer must be dense to protect the Cu substrate against oxidation/corrosion. Most manufacturers use a coating technology which intrinsically produces a dense layer (e.g. PECVD or natural oxide growth top layer)
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Acknowledgements



Aki Makilainen, Massoun Atfeh, Kaj Pischow, Rosa Aimò
(Savo-Solar, Mikkeli)

Luis Rebouta, Mikhail Vasilevskiy
(Uminho, Guimarães, Portugal)

Special thanks to the Organizers of **MIICS 2010**
